

Economic Fourth Order Three-stage Method for Solving Systems of Second Order Differential Equations with Special Structure

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Abstract—An explicit embedded pair of methods for systems of second order ordinary equations with special structure is considered. Two-parametric families of methods of orders four and three with automatic step-size control are constructed. The numeric comparison to known embedded Runge–Kutta pairs of the same order is held.

I. INTRODUCTION

In [1] for systems of the form

$$y'_i = f_i(x, y_1, \dots, y_{i-1}, y_{l+1}, \dots, y_n), \quad i = \overline{1, l}, \quad (1)$$

$$y'_j = f_j(x, y_1, \dots, y_{j-1}), \quad j = \overline{l+1, n}, \quad n \geq 3, \quad (2)$$

an economic embedded explicit Runge–Kutta type method with automatic step-size control was constructed. The method is of order 4 with order 3 error estimation and has 4 stages with the first stage for the group (1) being the same as the last of the previous step. The method is denoted as RKS4(3)4F with the denotation $RKSp(q)mF$ meaning Runge–Kutta type Structural method of order p with order q embedded estimator, with m stages and FSAL.

It was modified so that the error estimation is made only for functions of the group (1). So only three stages are required for the group (2) and effectively the method has just three stages for all unknown functions. Such modification is denoted RKS4(3)(4,3)F

Both methods have shown their effectiveness compared to the known embedded Runge–Kutta pairs of order 4 and 3. In general, methods for systems with special structure analogous to (1)–(2) are called *structural*. Methods for most general structure are considered in [2]–[4].

Here methods for direct integration of systems of second order equations of the form

$$\begin{cases} x'' = G(t, x, y, y'), \\ y'' = Q(t, x, y, x'). \end{cases} \quad (3)$$

are constructed on base of RKS4(3)4F and RKS4(3)(4,3)F. For example, the well-known restricted three-body problem is

described with such system. The equations [5]

$$\begin{aligned} x_1'' &= x_1 + 2x_2' - \mu' \frac{x_1 + \mu}{D_1} - \mu \frac{x_1 - \mu'}{D_2}, \\ x_2'' &= x_2 - 2x_1' - \mu' \frac{x_2}{D_1} - \mu \frac{x_2}{D_2}, \\ D_1 &= ((x_1 + \mu)^2 + x_2^2)^{3/2}, \quad D_2 = ((x_1 - \mu')^2 + x_2^2)^{3/2}, \\ \mu &= 0.012277471, \quad \mu' = 1 - \mu, \end{aligned} \quad (4)$$

rewritten with $y_1 = x_1', y_2 = x_2, y_3 = x_2', y_4 = x_1$ notations as a system of first-order equations, can be considered as a system (1)–(2) with $l = 2, n = 4$.

Since in the system (3) right-hand sides depend on first-derivatives special Runge–Kutta–Nyström methods (RKNs) for second-order equations are inapplicable, and direct application of standard Runge–Kutta methods cannot improve the stage to order ratio [6]. However it is possible to use structural methods for solving the system of first order equations derived from (3) and then rewrite them for direct application to the system of second order. This preserve the advantage of structural methods over classic Runge–Kutta methods.

II. INTEGRATION METHOD

To make the idea more clear we write down the method RKS4(3)(4,3)F for the system (3) in the full form. Assuming the values $x(t), x'(t), y(t)$ and $y'(t)$ known, the approximations X, X', Y and Y' to $x(t+h), x'(t+h), y(t+h)$ and $y'(t+h)$ are found as

$$\begin{aligned} X &= x(t) + hx'(t) + \frac{1}{10}hk_1^G + \frac{1}{3}hk_2^G + \frac{1}{15}hk_3^G, \\ X' &= x'(t) + \frac{1}{10}k_1^G + \frac{1}{2}k_2^G + \frac{2}{5}k_3^G, \\ Y &= y(t) + hy'(t) + \frac{1}{3}hk_1^Q + \frac{1}{6}hk_2^Q, \\ Y' &= y'(t) + \frac{2}{5}k_1^Q + \frac{1}{2}k_2^Q + \frac{1}{10}k_3^Q, \end{aligned} \quad (5)$$

where

$$\begin{aligned} k_1^G &= hG\left(t, x(t), y(t), y'(t)\right), \\ k_1^Q &= hQ\left(t + \frac{1}{6}h, x(t) + \frac{1}{6}hx'(t) + \frac{1}{36}hk_1^G, \right. \\ &\quad \left. y(t) + \frac{1}{6}hy'(t), x'(t) + \frac{1}{6}k_1^G\right), \\ k_2^G &= hG\left(t + \frac{1}{3}h, x(t) + \frac{1}{3}hx'(t) + \frac{1}{18}hk_1^G, \right. \\ &\quad \left. y(t) + \frac{1}{3}hy'(t) + \frac{1}{18}hk_1^Q, y'(t) + \frac{1}{3}k_1^Q\right), \end{aligned} \quad (6)$$

$$\begin{aligned}
k_2^Q &= hQ\left(t + \frac{2}{3}h, x(t) + \frac{2}{3}hx' + \frac{5}{72}hk_1^G + \frac{1}{8}hk_2^G, \right. \\
&\quad \left. y(t) + \frac{2}{3}hy'(t) + \frac{1}{4}hk_1^Q, x'(t) - \frac{1}{12}k_1^G + \frac{3}{4}k_2^G\right), \\
k_3^G &= hG\left(t + \frac{5}{6}h, x(t) + \frac{5}{6}hx'(t) + \frac{5}{144}hk_1^G + \frac{5}{16}hk_2^G, \right. \\
&\quad \left. y(t) + \frac{5}{6}hy'(t) + \frac{5}{18}hk_1^Q + \frac{5}{72}hk_2^Q, \right. \\
&\quad \left. y'(t) + \frac{5}{12}k_1^Q + \frac{5}{12}k_2^Q\right), \\
k_3^Q &= hQ\left(t + h, x(t) + hx'(t) - \frac{1}{24}hk_1^G + \frac{5}{8}hk_2^G, \right. \\
&\quad \left. y(t) + hy'(t) + \frac{5}{36}hk_1^Q + \frac{5}{18}hk_2^Q, \right. \\
&\quad \left. x'(t) + \frac{3}{4}k_1^G - \frac{5}{12}k_2^G + \frac{2}{3}k_3^G\right).
\end{aligned} \tag{7}$$

In order to find the local error estimation the value

$$k_4^G = hG(t + h, X, Y, Y') \tag{8}$$

is found and

$$\begin{aligned}
\bar{X} &= x(t) + hx'(t) + \left(\frac{1}{10} - \frac{2}{15}\eta\right)hk_1^G + \left(\frac{1}{3} + \frac{1}{6}\eta\right)hk_2^G \\
&\quad + \left(\frac{1}{15} + \frac{2}{15}\eta\right)hk_3^G - \frac{1}{6}\eta hk_4^G, \\
\bar{X}' &= x'(t) + \left(\frac{1}{10} - \frac{2}{5}\xi\right)k_1^G + \left(\frac{1}{2} + \xi\right)k_2^G \\
&\quad + \left(\frac{2}{5} - \frac{8}{5}\xi\right)k_3^G + \xi k_4^G, \\
\bar{Y} &= y(t) + hy'(t) + \left(\frac{1}{3} + \frac{1}{15}\xi\right)hk_1^Q \\
&\quad + \left(\frac{1}{6} - \frac{1}{6}\xi\right)hk_2^Q + \frac{1}{10}\xi hk_3^Q,
\end{aligned} \tag{9}$$

So

$$\begin{aligned}
x(t+h) &= X + O(h^5) = \bar{X} + O(h^4), \\
x'(t+h) &= X' + O(h^5) = \bar{X}' + O(h^4), \\
y(t+h) &= Y + O(h^5) = \bar{Y} + O(h^4), \\
y'(t+h) &= Y' + O(h^5).
\end{aligned}$$

The parameters η and ξ are non-zero and can be chosen arbitrarily. Let's denote the method (5)–(9) RKNS4(3)(4,3)F (though in fact it isn't an RKN).

In order to estimate the local error for all variables we need the value

$$\begin{aligned}
k_4^Q &= hQ\left(t + \frac{5}{6}h, \right. \\
&\quad \left. x(t) + \frac{5}{6}hx'(t) - \frac{1}{12}hk_1^G + \frac{1}{4}hk_2^G + \frac{1}{36}k_4^G, \right. \\
&\quad \left. y(t) + \frac{5}{6}hy'(t) + \frac{4}{15}hk_1^Q + \frac{1}{12}hk_2^Q - \frac{1}{60}k_3^Q, \right. \\
&\quad \left. x'(t) + \frac{1}{10}k_1^G + \frac{1}{2}k_2^G + \frac{2}{5}k_3^G - \frac{1}{6}k_4^G\right).
\end{aligned} \tag{10}$$

So it gives

$$\begin{aligned}
\bar{Y}' &= y'(t) + \left(\frac{2}{15} + \frac{1}{15}\eta\right)k_1^Q + \left(\frac{1}{2} - \frac{2}{3}\eta\right)k_2^Q \\
&\quad + \left(\frac{1}{10} - \frac{2}{5}\eta\right)k_3^Q + \eta k_4^Q,
\end{aligned} \tag{11}$$

which is order 3 approximation to $y'(t+h)$. Unfortunately k_4^Q cannot be reused at the next step. But still, the method (now denoted RKNS4(3)4F) is more effective than known methods.

III. TEST COMPUTATIONS

The methods were tested and compared on two problems.

Test 1. The methods RKNS4(3)4F and RKNS4(3)(4,3)F are compared to the classic four-stages RungeKutta method (“The” RungeKutta method) with five-stages third-order estimator, denoted RK4(3)T in [7], and to the same RungeKutta method but with an embedded second-order estimator (named in Russian mathematical tradition “Egorov control term” after Prof. Vsevolod A. Egorov [8] denoted RK4(2). They were used to solve the problem

$$x'' = -2x + \frac{1}{2}y', \quad y'' = -\frac{1}{2}x' - 2y, \tag{12}$$

$$x(0) = x'(0) = 1, \quad y(0) = 2, \quad y'(0) = 3,$$

in the interval $t \in [0, 2\pi]$. The general solution of (12) is

$$\begin{aligned}
x(t) &= C_1 \cos(\alpha t) + C_2 \sin(\alpha t) + C_3 \cos(\beta t) + C_4 \sin(\beta t), \\
y(t) &= -C_1 \sin(\alpha t) + C_2 \cos(\alpha t) - C_3 \sin(\beta t) + C_4 \cos(\beta t), \\
\alpha &= \frac{1 - \sqrt{33}}{4}, \quad \beta = \frac{1 + \sqrt{33}}{4}.
\end{aligned}$$

The effectiveness of any method depends on the algorithm of step-size control, and all the methods RKNS4(3)4F, RKNS4(3)(4,3)F and RK4(3)T, RK4(2) are of the same class of one-step methods. So all of them were realised with the similar algorithmic core. The new step-size was calculated as $h_{\text{new}} = 0.9 \cdot h(\text{tol}/\text{err})^{1/(q+1)}$, where tol is the local error tolerance and err is the measured local error.

The problem was solved with different tolerance values so that the global error δ changed from 10^{-6} to $10^{-11.5}$. All four methods showed the expected convergence, but it should be noted that the step-size control was more sensitive in case of RKNS4(3)4F and RKNS4(3)(4,3)F.

In the Table I the number of steps N_h and the number of right-hand side calculations N_{G+Q} over the whole interval $[0, 2\pi]$ which provide the norm of global error $\|\delta\|$ are given.

TABLE I
COMPARISON FOR THE TEST PROBLEM 1.

$\log_{10} \ \delta\ $	RKNS4(3)4F		RKNS4(3)(4,3)F		RK4(3)T		RK4(2)	
	N_h	N_{G+Q}	N_h	N_{G+Q}	N_h	N_{G+Q}	N_h	N_{G+Q}
−6.00	156	1 092	161	966	234	1 872	236	1 888
−6.50	211	1 477	218	1 308	310	2 480	312	2 480
−7.00	279	1 953	292	1 752	413	3 304	417	3 386
−7.50	377	2 639	395	2 370	553	4 424	556	4 444
−8.00	496	3 472	524	3 144	734	5 872	738	5 904
−8.50	661	4 627	708	4 248	978	7 824	983	7 864
−9.00	881	6 167	955	5 730	1 304	10 432	1 311	10 448
−9.50	1 174	8 218	1 280	7 680	1 737	13 896	1 747	13 976
−10.00	1 567	10 969	1 740	10 440	2 321	18 568	2 332	18 656
−10.50	2 087	14 609	2 325	13 950	3 089	24 712	3 106	24 848
−11.00	2 783	19 481	3 110	18 660	4 116	32 928	4 141	33 128
−11.50	3 712	25 984	4 172	25 032	5 490	43 920	5 522	44 176

The results confirm theoretical expectations. The global error to right-hand side computations ratio show that for the

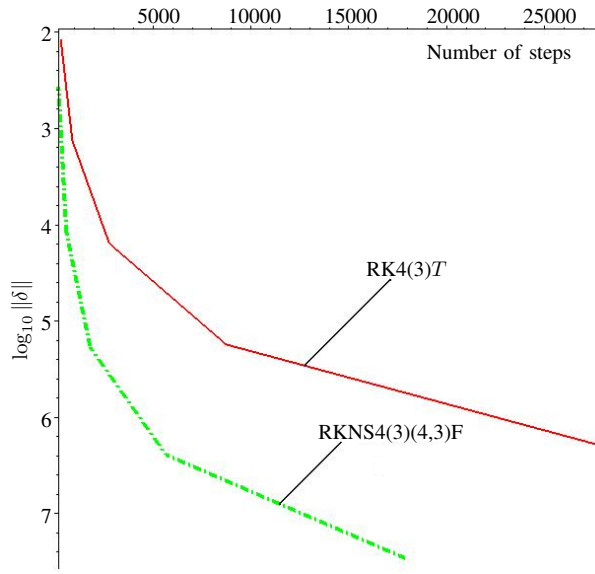


Fig. 1. Global error to number of steps ratio comparison in Test 2.

same $\|\delta\|$ values RKNS4(3)4F and RKNS4(3)(4,3)F demand fewer steps and right-hand side evaluations. And for the same computational cost RK4(3)T and RK4(2) are less effective than RKNS4(3)4F and RKNS4(3)(4,3)F in sense of global error value.

Test 2. The restricted three-body problem (4) with specially chosen initial values, for example

$$\begin{aligned} x_1(0) &= 0.994, & x_1'(0) &= 0, & x_2(0) &= 0, \\ x_2'(0) &= 2.00158510637908252240537862224, \\ t_{\text{end}} &= 17.0652165601579625588917206249, \end{aligned} \quad (13)$$

has periodic solution with period t_{end} [6]. Such orbits are often called “Arenstorf orbits”. The initial value problem was solved up to t_{end} with RKNS4(3)(4,3)F with $\xi = \eta = 3$ (in form (3)) and with RK4(3)T (in form (1)–(2)) and the deviation in the end from the initial value was measured, being used as a global error δ evaluation.

In the Figure 1 the global error to the number of steps ratio for both methods are presented. RKNS4(3)(4,3)F provides the same accuracy with fewer steps, and moreover takes fewer stages per step. This confirms, as it was expected by the construction, its better performance in comparison with classic Runge–Kutta schemes.

IV. CONCLUSION

The numeric tests confirm that methods exploiting special structure of ODE systems are more effective. Specially constructing them with different computational schemes for different parts of systems one can obtain the demanded convergence order and global error with fewer stages than with usual Runge–Kutta methods.

Direct implementation of such methods to systems of second-order equations keeps the mentioned effectiveness. Their field of application is wider than of known Runge–Kutta–Nyström methods.

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